

# **GEOTECHNICAL INVESTIGATION**

**FOR** 

# **NSW Land & Housing Corporation**

189 Riverside Drive, Airds, New South Wales

Report No: 20/1924

Project No: 30553/3990D-G

June 2020



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## 1. INTRODUCTION

This report presents the results of a Geotechnical Investigation carried out by STS Geotechnics Pty Limited (STS) for a proposed new residential development to be constructed at 189 Riverside Drive, Airds. At the time of writing this report STS were not provided with architectural drawings for the project, however we understand the development will typically comprise the demolition of existing dwellings and construction of one to two level residential unit type buildings. The development will not include basement levels.

The purpose of the investigation was to:

- assess the subsurface conditions over the site,
- provide a Site Classification to AS2870,
- provide recommendations regarding the appropriate foundation system for the site including design parameters, and
- comment on soil aggressiveness to buried steel and concrete.

The investigation was undertaken at the request of Land and Housing Corporation NSW.

Our scope of work did not include a contamination assessment.

## 2. NATURE OF THE INVESTIGATION

## 2.1. Fieldwork

The fieldwork consisted of drilling three (3) boreholes numbered BH1 to BH3, at the locations shown on Drawing No. 20/1924. The boreholes were drilled using a track mounted Mini Christie drilling rig owned and operated by STS. Soils and weathered bedrock were drilled using rotary solid flight augers. Soil strengths were determined by undertaking Dynamic Cone Penetrometer (DCP) tests at each borehole location.

Drilling operations were undertaken by one of STS's senior geologists who also logged the subsurface conditions encountered.

The subsurface conditions observed are recorded on the borehole logs given in Appendix A. An explanation of the terms used on the logs is also given in Appendix A. Notes relating to geotechnical reports are also attached.

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## 2.2. Laboratory Testing

In order to assist with determining the site classification, shrink swell index tests were carried out on representative samples retrieved from the site.

In order to assess the soils for their aggressiveness, selected representative soil samples were tested to determine the following:

- pH,
- Sulphate content (SO<sub>4</sub>),
- Chloride content (CL), and
- Electrical Conductivity (EC)

Detailed test reports are given in Appendix B.

## 3. GEOLOGY AND SITE CONDITIONS

The Wollongong – Port Hacking geological series sheet at a scale of 1:100,000 indicates Triassic Age Hawkesbury Sandstone underlies the site. Rocks within this formation comprise fine to medium grained quartz sandstone.

The site is roughly trapezoidal in shape with a combined area of approximately 640 m<sup>2</sup>. At the time of the fieldwork, the site was vacant. Site vegetation comprised grass, trees and shrubs.

The ground surface falls approximately 0.8 metres to the north-east.

To the south-east and south-west of the site are Riverside Drive and Elizabeth Walk respectively, and to the remaining sides are single storey residential dwellings.

## 4. SUBSURFACE CONDITIONS

When assessing the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour regarding the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies.

The subsurface conditions generally consist of topsoil and fill overlying natural silty clays and weathered sandstone. Some organics and minor topsoil and fill were encountered at the ground surface to approximate depths of 0.2 to 0.3 metres. Natural silty clays of firm becoming stiff and very stiff consistency were encountered below the surface materials to approximate depths of 1.2 and 2.5 m. The firm clays were only encountered in BH1 and to a depth of 0.6 metres. Weathered sandstone bedrock underlies the soils and was encountered to the depth of drilling, 3.0 metres.

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Groundwater was not observed during drilling of the boreholes.

## 5. GEOTECHNICAL DISCUSSION

## 5.1. Site Classification to AS2870

The classification has been prepared in accordance with the guidelines set out in the "Residential Slabs and Footings" Code, AS2870 – 2011.

An undisturbed sample was collected from BH1 to determine the soils Shrink Swell Index. The result of the testing is summarised in Table 5.1 below:

Table 5.1 – Shrink Swell Summary Table

Location	Depth (m)	Material Description	Shrink/Swell Index (% per ∆pF)
BH1	0.5 - 0.7	Red brown with light grey silty clay	2.2

Because there are trees present, abnormal moisture conditions (AMC) prevail at the site (Refer to Section 1.3.3 of AS2870).

Because of the AMC, the site is classified *a problem site* (*P*). However, provided the recommendations given below are adopted and the footings bear in the underlying natural soils, the site may be reclassified *Highly Reactive* (*H1*).

## 5.2. Foundation Design

Footings that bear in the firm natural clayey soils below any topsoil or fill may be proportioned using an allowable bearing pressure of 70 kPa. This value may be increased to 100 kPa in firm to stiff clays. The minimum depth of founding must comply with the requirements of AS2870-2011. The structural designer should also be aware that the standard designs given in AS2870 assume a minimum allowable bearing pressure of 100 kPa.

In order to overcome the presence of trees, the foundations should be designed in accordance with the procedures given in Appendices H and CH of AS2870-2011. Tree information is attached.

Piers or footings founded in very stiff clays may be proportioned using an allowable bearing pressure of 300 kPa. An allowable adhesion of 20 kPa may be adopted for the portion of the shaft within the natural soils.

Piles founded in weathered sandstone may be proportioned using an allowable bearing pressure of 800 kPa. An allowable adhesion of 80 kPa may be adopted for the portion of the shaft within the weathered sandstone. When piles are founded in rock the adhesion within the overlying soils must be ignored.

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In order to ensure the bearing values given can be achieved, care should be taken to ensure that the base of excavations are free of all loose material prior to concreting. It is recommended that all footing excavations be protected with a layer of blinding concrete as soon as possible, preferably immediately after excavating, cleaning, inspection and approval. The possible presence of groundwater needs to be considered when drilling piers and pouring concrete.

## 5.3. Soil Aggressiveness

The aggressiveness or erosion potential of an environment in building materials, particularly concrete and steel is dependent on the levels of soil pH and the types of salts present, generally sulphates and chlorides. In order to determine the degree of aggressiveness, the test values obtained are compared to Tables 6.4.2 (C) and 6.5.2 (C) in AS2159 - 2009 Piling - Design and Installation and Tables 5.1 and 5.2 of AS2870-2011. In regards to the electrical conductivity, the laboratory test result has been multiplied by the appropriate factor to convert the result to EC<sub>e</sub>. The test results are summarised in Table 5.2 below.

Table 5.2 - Soil Aggressiveness Summary Table

Sample No.	Location	Depth (m)	рН	Sulfate (mg/kg)	Chloride (mg/kg)	Elect Condu (dS	ıctivity
						EC <sub>1:5</sub>	ECe
S1	BH1	0.3	5.3	80	90	0.095	0.7

The soils on the site consist of low permeability silty clays. Therefore, the soil conditions B are considered appropriate.

A review of the durability aspects indicates that:

• pH : minimum value of 5.3

SO<sub>4</sub> : maximum value of 80 mg/kg (ppm) < 5000 ppm</li>
 Cl : maximum value of 90 mg/kg (ppm) < 5000 ppm</li>

EC<sub>e</sub> : maximum value of 0.7 dS/m

The exposure classification for the onsite soils is non-aggressive for steel and mildly aggressive to concrete in accordance with AS2159-2009. The soils are classified as A2 in accordance with AS2870-2011.

Reference to DLWC (2002) "Site Investigations for Urban Salinity" indicates that an EC<sub>e</sub> value of 0.7 dS/m is consistent with the presence of non-saline soils.

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## 6. FINAL COMMENTS

During construction, should the subsurface conditions vary from those inferred above, we would be contacted to determine if any changes should be made to our recommendations.

The exposed bearing surfaces for footings should be inspected by a geotechnical engineer to ensure the allowable pressure given has been achieved.

Rasoul Machiani Senior Geotechnical Engineer

STS Geotechnics Pty Limited

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Matthew Green
Principal Engineering Geologist
STS Geotechnics Pty Limited

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Scale: Unknown

Date: June 2020

Client: NSW LAND & HOUSING CORPORATION

GEOTECHNICAL INVESTIGATION
189 RIVERSIDE DRIVE, AIRDS
BOREHOLE AND PENETROMETER LOCATIONS

Project No. 30553/3990D-G

Drawing No: 20/1924

#### NOTES RELATING TO GEOTECHNICAL REPORTS

#### Introduction

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report.

When copies of reports are made, they should be reproduced in full.

## **Geotechnical Reports**

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by STS Geotechnics Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions.
   The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, STS Geotechnics Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

#### **Unforeseen Conditions**

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, STS Geotechnics Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows reinterpretation and assessment of the implications for future work.

#### **Subsurface Information**

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

# **Supply of Geotechnical Information or Tendering Purposes**

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.



# APPENDIX A – BOREHOLE LOGS AND EXPLANATION SHEETS

## **GEOTECHNICAL LOG - NON CORE BOREHOLE**

	NSW Land & 89 Riverside I	Housing Corpor	Project / STS No. 30553/3990D-G  Date: June 18, 2020	В	OREHOLE NO.:	BH 1
		ving No. 20/192			Sheet 1 of 1	
W ATTA EBRL E	S A M P L E	<b>DEPTH</b> (m)	DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
		<del></del>	TOPSOIL: SILTY CLAY: dark brown, medium plasticity	CL	SOFT TO FIRM	М
			SILTY CLAY: red brown with light grey, high plasticity	СН	FIRM	М
	S1 @ 0.3 m	0.5				
	U50				FIRM TO STIFF	-
		1.0	SILTY CLAY: light grey with orange brown and red brown, medium to high plasticity, trace of ironstone gravel	CL/CH	STIFF	М
			SILTY CLAY: light grey with red brown, medium to high plasticity, trace of ironstone gravel	CL/CH	STIFF	M-D
		<u></u>				
		1.5				
					VERY STIFF	
		2.0				
		2.0				
			WEATHERED SANDSTONE: dark brown/orange brown with light grey, fine grained,		EXTREMELY	D
			clay seams		LOW STRENGTH	
		2.5				
			PODEHOLE DISCONTINUED AT 2.0 M ON WEATHERED CANDSTONE			
	D - disturbe		BOREHOLE DISCONTINUED AT 3.0 M ON WEATHERED SANDSTONE  U - undisturbed tube sample B - bulk sample	Contractor	: STS	<u> </u>
		f water table or			:: Mini Christie	
	S - jar samp	le		Hole Diam	eter (mm): 100	
NOTES:			See explanation sheets for meaning of all descriptive terms and symbols	Angle from	Vertical (°): 0	
				Drill Bit: S	piral	

Revision: 1

## **GEOTECHNICAL LOG - NON CORE BOREHOLE**

Revision: 1

	NSW Land & 89 Riverside I	Housing Corpor	ration Project / STS No. 30553/3990D-G Date: June 18, 2020	В	OREHOLE NO.:	BH 2
-		ving No. 20/192			Sheet 1 of 1	
W AT TA EB RL	S A M P L E S	<b>DEPTH</b> (m)	<b>DESCRIPTION OF DRILLED PRODUCT</b> (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			FILL: SILTY CLAY: light brown/orange brown, medium plasticity, trace of gravel	CL	FIRM TO STIFF	D-M
		0.5	SILTY CLAY: red brown with light grey, high plasticity	СН	STIFF	D-M
			SILTY CLAY: light grey with orange brown, medium to high plasticity, trace of ironstone gravel	CL/CH	STIFF	D-M
		1.0				
		1.5				
					VERY STIFF	
		2.0				
		2.5				
			WEATHERED SANDSTONE: light grey with orange brown, fine grained		EXTREMELY LOW STRENGTH	D
			AUGER REFUSAL AT 2.7 M ON WEATHERED SANDSTONE			
	D - disturbe	d samnle	U - undisturbed tube sample B - bulk sample	Contractor	· STS	
		f water table or	·		: Mini Christie	
NOTES:	S - jar samp	le			eter (mm): 100 Vertical (°): 0	
				Orill Bit: S	piral	

## **GEOTECHNICAL LOG - NON CORE BOREHOLE**

	NSW Land & 89 Riverside	Housing Corpo	ration	В	OREHOLE NO.:	BH 3
-		ving No. 20/19			Sheet 1 of 1	
W ATTA EBRL E	S A M P L E	<b>DEPTH</b> (m)	<b>DESCRIPTION OF DRILLED PRODUCT</b> (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			TOPSOIL: SILTY CLAY: dark brown, medium plasticity	CL	FIRM TO STIFF	М
			SILTY CLAY: red brown with light grey, high plasticity	СН	FIRM TO STIFF	M
			SELT CEAT. Ted brown with light grey, high plasticity	Сп	FIRIW TO STIFF	IVI
		0.5			STIFF	
			SILTY CLAY: light grey with orange brown, medium to high plasticity, trace of sandstone gravel	CL/CH	VERY STIFF	M-D
		1.0				
			WEATHERED SANDSTONE: light grey, fine grained		EXTREMELY LOW STRENGTH	D
		1.5				
			AUGER REFUSAL AT 1.5 M ON WEATHERED SANDSTONE			
		2.0				
		2.5				
		_				
	D - disturbe WT - level o	d sample f water table o	·	Contractor Equipment	: STS : Mini Christie	
	S - jar samp				eter (mm): 100	
NOTES:				Angle from Drill Bit: Sp	Vertical (°): 0	
				וט ייייט וויי	ui	

14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Report No.: 20/1924

## Dynamic Cone Penetrometer Test Report

Project: 189 RIVERSIDE DRIVE, AIRDS Project No.: 30553/3990D-G

Client: NSW LAND & HOUSING CORPORATION

Address: 31-39 Macquarie Street, Parramatta

Test Method: AS 1289.6.3.2

Accredited for compliance with ISO/IEC

17025 - Testing

The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards NATA Accreditation Number 2750

Report Date: 23/06/2020 Page: 1 of 1

Site No.	P1	P2	Р3			
Location	Refer to Drawing No. 20/1924	Refer to Drawing No. 20/1924	Refer to Drawing No. 20/1924			
Date Tested	18/6/2020	18/6/2020	18/6/2020			
Starting Level	Surface Level	Surface Level	Surface Level			
Depth (m)		Pe	netration Resistar	nce (blows / 150m	m)	
0.00 - 0.15	2	4	2			
0.15 - 0.30	1	6	3			
0.30 - 0.45	2	7	4			
0.45 - 0.60	2	7	4			
0.60 - 0.75	3	8	6			
0.75 - 0.90	3	10	10			
0.90 - 1.05	5	13	18			
1.05 - 1.20	8	12	22			
1.20 - 1.35	7	9	Refusal			
1.35 - 1.50	10	8				
1.50 - 1.65	9	11				
1.65 - 1.80	12	22				
1.80 - 1.95	15	Refusal				
1.95 - 2.10	22					
2.10 - 2.25	Refusal					
2.25 - 2.40						
2.40 - 2.55						
2.55 - 2.70						
2.70 - 2.85						
2.85 - 3.00						
3.00 - 3.15						
3.15 - 3.30						
3.30 - 3.45						
3.45 - 3.60						
3.60 - 3.75						

Remarks: \* Pre drilled prior to testing

Approved Signatory.....

Technician: JK Orlando Mendoza - Laboratory Manager

Form: RPS26 Date of Issue: 1/10/19 Revision: 1

. 14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



## Tree Heights and Type

Project: 189 Riverside Drive, Airds Project No. / STS No.: 30555/3990D-G

lient: NSW Land & Hous	ing Corporation	T	<del></del>	Technician:	JK I	<u></u>
Tree No.	Canopy Radius	Distance from Tree Along Ground	Uphill / Level / Downhill	Height of Tree	Native	Growing/Mature
	(m)	(m)		(m)	(Y/N)	
T1	3		U	12	N	G
T2	5		L	22	Υ	М
Т3	3		D	15	Υ	G
Numerous Trees and Shrubs						
		I	1			

#### E1. CLASSIFICATION OF SOILS

# E1.1 Soil Classification and the Unified System

An assessment of the site conditions usually includes an appraisal of the data available by combining values of engineering properties obtained by the site investigation with descriptions, from visual observation of the materials present on site.

The system used by STS Geotechnics Pty Ltd (STS) in the identification of soil is the Unified Soil Classification system (USC) which was developed by the US Army Corps of Engineers during World War II and has since gained international acceptance and has been adopted in its metricated form by the Standards Association of Australia.

The Australian Site Investigation Code (AS1726-1981, Appendix D) recommends that the description of a soil includes the USC group symbols which are an integral component of the system.

The soil description should contain the following information in order:

#### Soil composition

- SOIL NAME and USC classification symbol (IN BLOCK LETTERS)
- plasticity or particle characteristics
- colour
- secondary and minor constituents (name estimated proportion, plasticity or particle characteristics, colour

#### Soil condition

- moisture condition
- consistency or density index

#### Soil structure

• structure (zoning, defects, cementing)

#### Soil origin

interpretation based on observation eg FILL, TOPSOIL, RESIDUAL, ALLUVIUM.

E1.2 Soil Composition

(a) Soil Name and Classification Symbol

The USC system is summarised in Figure E1.2.1. The primary division separates soil types on the basis of particle size into:

- Coarse grained soils more than 50% of the material less than 60 mm is larger than 0.06 mm (60 μm).
- Fine grained soils more than 50% of the material less than 60 mm is smaller than 0.06 mm (60  $\mu$ m).

Initial classification is by particle size as shown in Table E1.2.1. Further classification of fine grained soils is based on plasticity.

TABLE E1.2.1 - CLASSIFICATION BY PARTICLE SIZE

NAME	SUB-DIVISION	SIZE
Clay (1)		< 2 μm
Silt (2)		2 μm to 60 μm
Sand	Fine Medium Coarse	60 μm to 200 μm 200 μm to 600 μm 600 μm to 2 mm
Gravel (3)	Fine Medium Coarse	2 mm to 6 mm 6 mm to 20 mm 20 mm to 60 mm
Cobbles (3)		60 mm to 200 mm
Boulders (3)		> 200 mm

Where a soil contains an appropriate amount of secondary material, the name includes each of the secondary components (greater than 12%) in increasing order of significance, eg sandy silty clay.

Minor components of a soil are included in the description by means of the terms "some" and "trace" as defined in Table E1.2.2.

TABLE E1.2.2 - MINOR SOIL COMPONENTS

TERM	DESCRIPTION	APPROXIMATE PROPORTION (%)
Trace	presence just detectable, little or no influence on soil properties	0-5
Some	presence easily detectable, little influence on soil properties	5-12

The USC group symbols should be included with each soil description as shown in Table E1.2.3

TABLE E1.2.3 - SOIL GROUP SYMBOLS

SOIL TYPE	PREFIX
Gravel	G
Sand	S
Silt	M
Clay	С
Organic	О
Peat	Pt

The group symbols are combined with qualifiers which indicate grading, plasticity or secondary components as shown on Table E1.2.4

TABLE E1.2.4 - SOIL GROUP QUALIFIERS

SUBGROUP	SUFFIX
Well graded	W
Poorly Graded	P
Silty	M
Clayey	C
Liquid Limit <50% - low to medium plasticity	L
Liquid Limit >50% - medium to high plasticity	Н

#### (b) Grading

"Well graded" Good representation of all

particle sizes from the largest

to the smallest.

"Poorly graded" One or more intermediate

sizes poorly represented

"Gap graded" One or more intermediate

sizes absent

"Uniformly graded" Essentially single size

material.

#### (c) Particle shape and texture

The shape and surface texture of the coarse grained particles should be described.

**Angularity** may be expressed as "rounded", "subrounded", "sub-angular" or "angular".

Particle **form** can be "equidimensional", "flat" or elongate".

**Surface texture** can be "glassy", "smooth", "rough", pitted" or striated".

#### (d) Colour

The colour of the soil should be described in the moist condition using simple terms such as:

Black White Grey Red Brown Orange Yellow Green Blue

These may be modified as necessary by "light" or "dark". Borderline colours may be described as a combination of two colours, eg red-brown.

For soils that contain more than one colour terms such as:

• Speckled Very small (<10 mm dia) patches

• Mottled Irregular

• Blotched Large irregular (>75 mm dia)

• Streaked Randomly oriented streaks

#### (e) Minor Components

Secondary and minor components should be individually described in a similar manner to the dominant component.

#### E1.3 Soil Condition

#### (a) Moisture

Soil moisture condition is described as "dry", "moist" or "wet".

The moisture categories are defined as:

Dry (D) - Little or no moisture evident. Soils are running. Moist (M) - Darkened in colour with cool feel. Granular soil particles tend to adhere. No free water evident upon remoulding of cohesive soils.

In addition the moisture content of cohesive soils can be estimated in relation to their liquid or plastic limit.

#### (b) Consistency

Estimates of the consistency of a clay or silt soil may be made from manual examination, hand penetrometer test, SPT results or from laboratory tests to determine undrained shear or unconfined compressive strengths. The classification of consistency is defined in Table E1.3.1.

TABLE E1.3.1 - CONSISTENCY OF FINE-GRAINED SOILS

TERM	UNCONFINED STRENGTH (kPa)	FIELD IDENTIFICATION
Very Soft	<25	Easily penetrated by fist. Sample exudes between fingers when squeezed in the fist.
Soft	25 - 50	Easily moulded in fingers. Easily penetrated 50 mm by thumb.
Firm	50 - 100	Can be moulded by strong pressure in the fingers. Penetrated only with great effort.
Stiff	100 - 200	Cannot be moulded in fingers. Indented by thumb but penetrated only with great effort.
Very Stiff	200 - 400	Very tough. Difficult to cut with knife. Readily indented with thumb nail.
Hard	>400	Brittle, can just be scratched with thumb nail. Tends to break into fragments.

Unconfined compressive strength as derived by a hand penetrometer can be taken as approximately double the undrained shear strength  $(q_u = 2 \ c_u)$ .

## (c) Density Index

The insitu density index of granular soils can be assessed from the results of SPT or cone penetrometer tests. Density index should not be estimated visually.

TABLE E1.3.2 - DENSITY OF GRANULAR SOILS

TERM	SPT N	STATIC	DENSITY	
	VALUE	CONE	INDEX	
		VALUE	(%)	
		q <sub>c</sub> (MPa)		
Very Loose	0 - 3	0 - 2	0 - 15	
Loose	3 - 8	2 - 5	15 - 35	
Medium Dense	8 - 25	5 - 15	35 - 65	
Dense	25 - 42	15 - 20	65 - 85	
Very Dense	>42	>20	>85	

#### E1.4 Soil Structure

#### (a) Zoning

A sample may consist of several zones differing in colour, grain size or other properties. Terms to classify these

Layer - continuous across exposure or sample

Lens - discontinuous with lenticular shape

Pocket - irregular inclusion

Each zone should be described, their distinguishing features, and the nature of the interzone boundaries.

#### (b) Defects

Defects which are present in the sample can include:

- fissures
- roots (containing organic matter)
- tubes (hollow)
- · casts (infilled)

Defects should be described giving details of dimensions and frequency. Fissure orientation, planarity, surface condition and infilling should be noted. If there is a tendency to break into blocks, block dimensions should be recorded

#### E1.5 Soil Origin

Information which may be interpretative but which may contribute to the usefulness of the material description should be included. The most common interpreted feature is the origin of the soil. The assessment of the probable origin is based on the soil material description, soil structure and its relationship to other soil and rock materials.

#### Common terms used are:

"Residual Soil" - Material which appears to have been derived by weathering from the underlying rock. There is no evidence of transport.

"Colluvium" - Material which appears to have been transported from its original location. The method of movement is usually the combination of gravity and erosion

"Landslide Debris" - An extreme form of colluvium where the soil has been transported by mass movement. The material is obviously distributed and contains distinct defects related to the slope failure.

"Alluvium" - Material which has been transported essentially by water. usually associated with former stream activity.

"Fill" - Material which has been transported and placed by man. This can range from natural soils which have been placed in a controlled manner in engineering construction to dumped waste material. A description of the constituents should include an assessment of the method of placement.

#### E1.6 Fine Grained Soils

The physical properties of fine grained soils are dominated by silts and clays.

The definition of clay and silt soils is governed by their Atterberg Limits. Clay soils are characterised by the properties of cohesion and plasticity with cohesion defines as the ability to deform without rupture. Silts exhibit cohesion but have low plasticity or are non-plastic.

The field characteristics of clay soils include:

- dry lumps have appreciable dry strength and cannot be powdered
- volume changes occur with moisture content variation
- feels smooth when moist with a greasy appearance when cut.

The field characteristics of silt soils include:

- dry lumps have negligible dry strength and can be powdered easily
- dilatancy an increase in volume due to shearing is indicted by the presence of a shiny film of water after a hand sample is shaken. The water disappears upon remoulding. Very fine grained sands may also exhibit dilatancy.
- low plasticity index
- feels gritty to the teeth

#### E1.7 Organic Soils

Organic soils are distinguished from other soils by their appreciable content of vegetable matter, usually derived from plant remains.

The soil usually has a distinctive smell and low bulk density.

The USC system uses the symbol Pt for partly decomposed organic material. The O symbol is combined with suffixes "O" or "H" depending on plasticity.

Where roots or root fibres are present their frequency and the depth to which they are encountered should be recorded. The presence of roots or root fibres does not necessarily mean the material is an "organic material" by classification.

Coal and lignite should be described as such and not simply as organic matter.



# APPENDIX B – LABORATORY TEST RESULTS



## **CERTIFICATE OF ANALYSIS**

**Work Order** : ES2021306

: STS Geotechnics

Contact : ENQUIRES STS

Address : Unit 14/1 Cowpasture Place

Wetherill Park 2164

Telephone

Client

Project : 30553/3554 Order number : E-2020-0223

C-O-C number Sampler Site Quote number : EN/222

No. of samples received : 4 No. of samples analysed : 4 Page : 1 of 2

Laboratory : Environmental Division Sydney

Contact : Customer Services ES

Address : 277-289 Woodpark Road Smithfield NSW Australia 2164

Telephone : +61-2-8784 8555

**Date Samples Received** : 19-Jun-2020 11:50

**Date Analysis Commenced** : 23-Jun-2020

Issue Date : 24-Jun-2020 18:11



This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with **Quality Review and Sample Receipt Notification.** 

#### Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories	Position	Accreditation Category	
Ashesh Patel	Senior Chemist	Sydney Inorganics, Smithfield, NSW	

Sydney Inorganics, Smithfield, NSW Dian Dao Ivan Taylor

Page : 2 of 2 Work Order : ES2021306

Client : STS Geotechnics

Project : 30553/3554



## **General Comments**

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

- ^ = This result is computed from individual analyte detections at or above the level of reporting
- ø = ALS is not NATA accredited for these tests.
- ~ = Indicates an estimated value.

### Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)	Client sample ID			30553/S1	30554/S1	30554/S2	30554/S3	
Client sampling date / time			18-Jun-2020 00:00	18-Jun-2020 00:00	18-Jun-2020 00:00	18-Jun-2020 00:00		
Compound	CAS Number	LOR	Unit	ES2021306-001	ES2021306-002	ES2021306-003	ES2021306-004	
				Result	Result	Result	Result	
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	5.3	6.5	6.5	5.7	
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	μS/cm	95	76	47	100	
EA055: Moisture Content (Dried @ 105-11	10°C)							
Moisture Content		0.1	%	21.4	20.1	21.3	18.1	
ED040S : Soluble Sulfate by ICPAES								
Sulfate as SO4 2-	14808-79-8	10	mg/kg	80	100	20	150	
ED045G: Chloride by Discrete Analyser								
Chloride	16887-00-6	10	mg/kg	90				